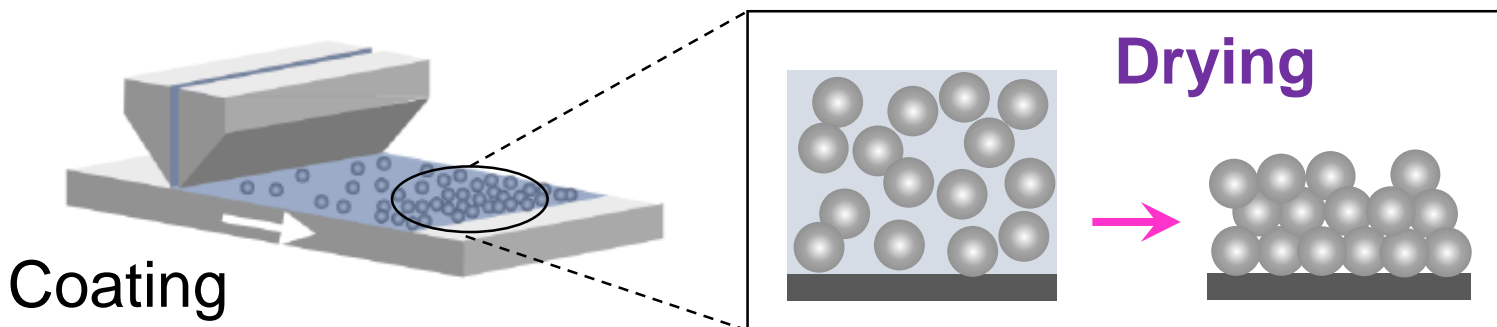


Estimation of the drying characteristics of colloidal suspensions by numerical simulation

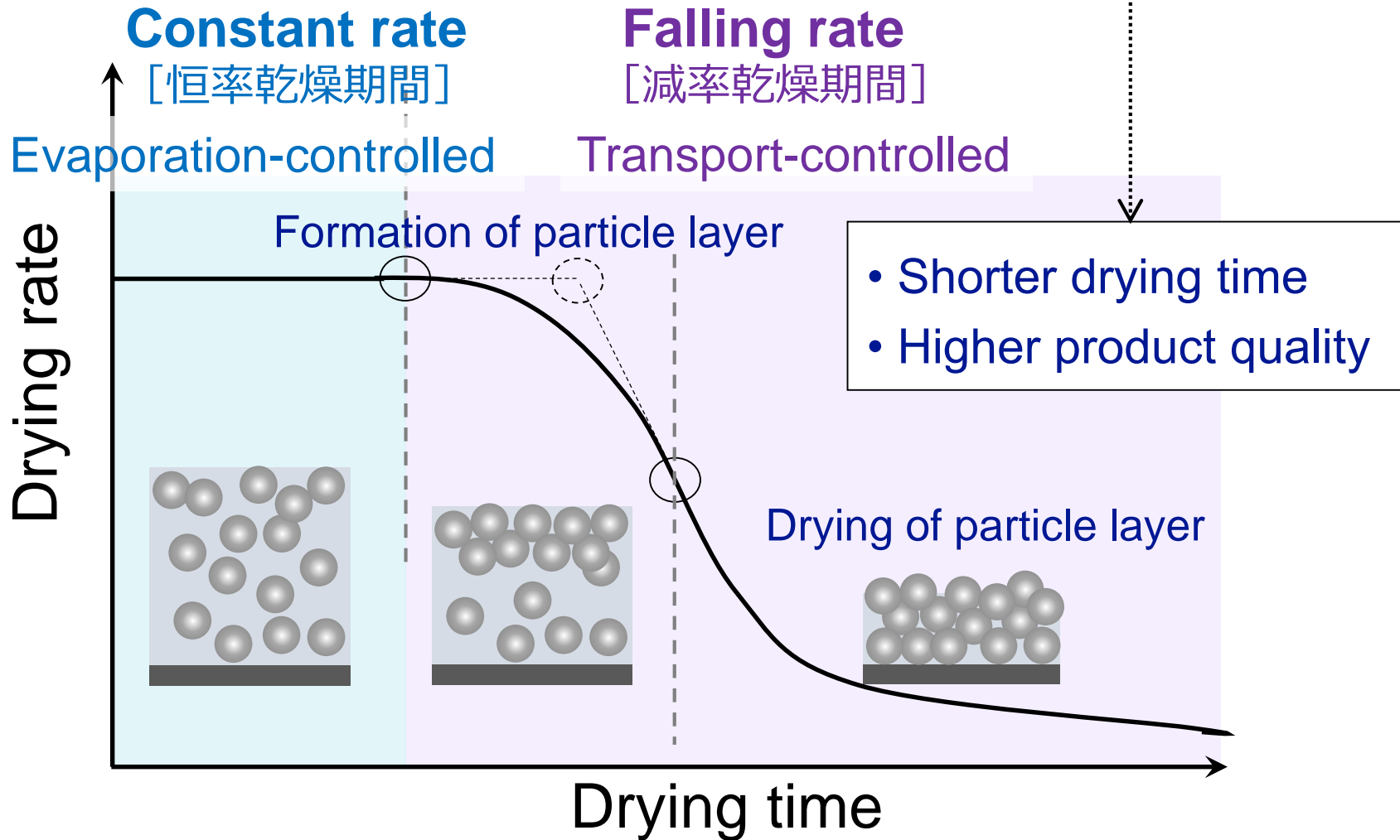
数値シミュレーションによる微粒子分散液の乾燥特性の予測

- 辰巳 怜 (東大環安セ)
- 小池 修 (PIA)
- 山口由岐夫 (PIA)
- 辻 佳子 (東大環安セ/東大院工)



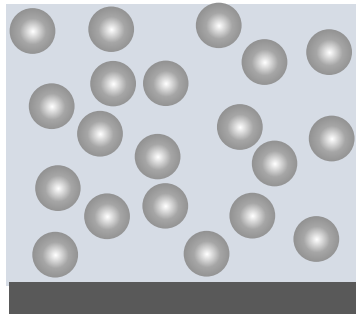
Drying Curve of Colloidal Suspensions

Drying characteristics ↔ Structure

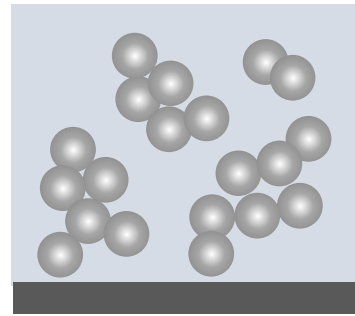


Objective

- ◆ Estimation of the drying curve of colloidal suspensions by numerical simulation (SNAP-L)
- ◆ Effects of particle dispersion/aggregation on the drying curve



Dispersion

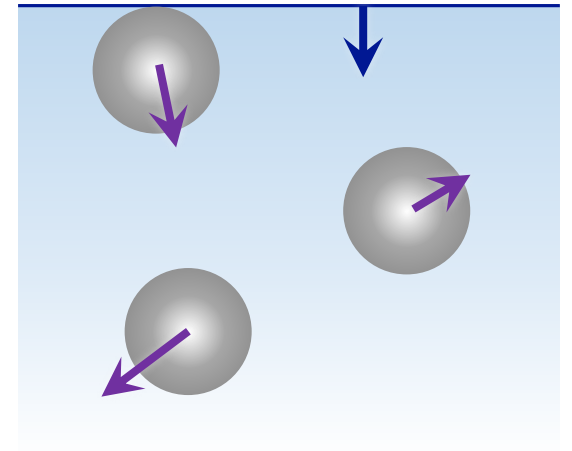
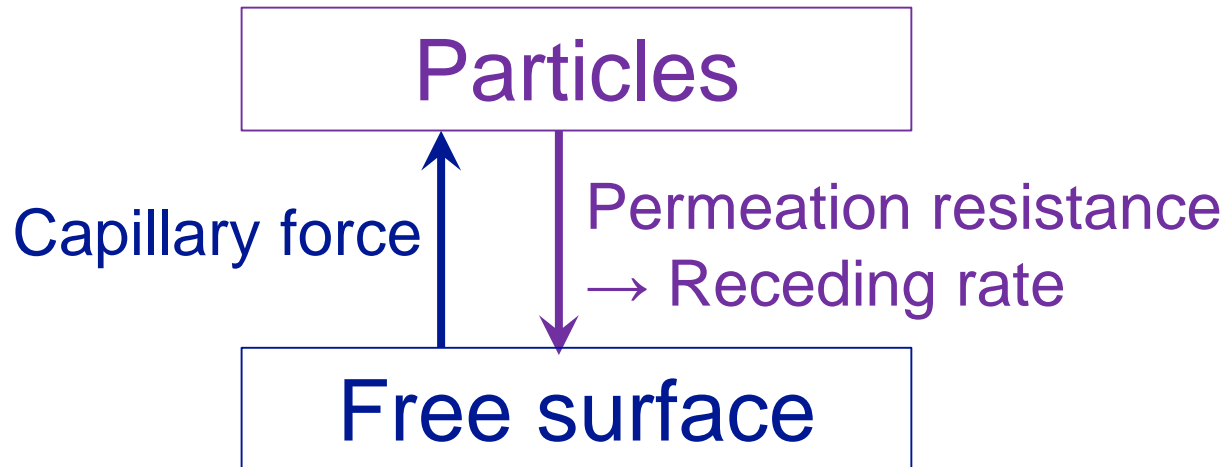


Aggregation

Drying characteristics \leftrightarrow Structure

Model

- **Particles:** Equation of motion (Langevin eq.)
- **Free surface:** Recession with a varying rate



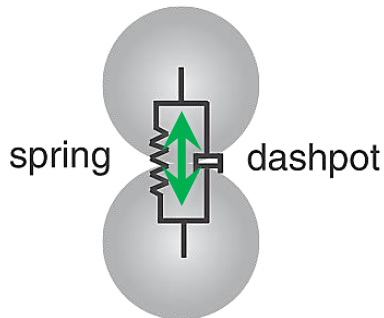
Particles' Brownian Motion

Langevin equation

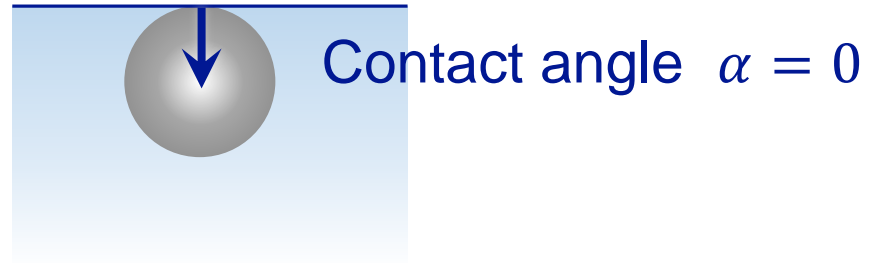
$$M_i \dot{V}_i = -\xi V_i + \underbrace{F_i^R}_{\text{Fluid}} + \underbrace{F_i^{\text{cnt}}}_{\text{Interparticle}} + \underbrace{F_i^{\text{cpl}}}_{\text{Free surface}}$$

- **Drag force:** $-\xi V_i$ Stokes' law: $\xi = 3\pi\eta d$
 - **Random force:** $F_{i\alpha}^R(t) \sim N(0, 2\xi k_B T \Delta t)$ (Gaussian dist.)
- **Brownian Diffusion:** $D = \frac{k_B T}{3\pi\eta d}$ Diffusion coefficient

- **Contact force:** F_i^{cnt}



- **Vertical capillary force:** F_i^{cpl}



Drying Rate

Darcy's law

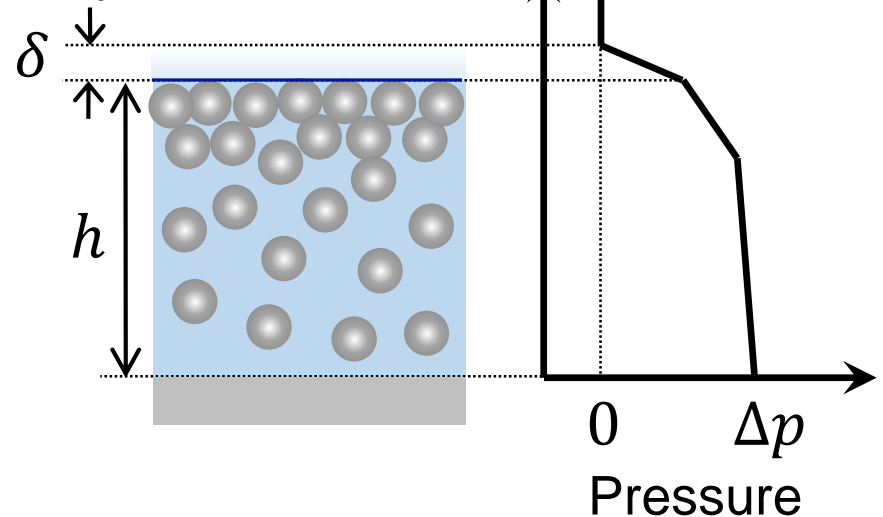
$$\text{Drying rate: } u = \frac{\Delta p}{\eta(R_0 + R_p)}$$

Resistance of evaporation: R_0

Resistance of suspensions: R_p

Viscosity of liquid: η

Boundary film



Resistance of evaporation

Drying rate of the liquid containing no particles:

$$u_0 = \frac{D_v}{\delta} \frac{v_1}{k_B T} \Delta p = \frac{\Delta p}{\eta R_0}$$

Diffusion coefficient of vapor: D_v

Molecular volume of liquid: v_1

Drying Rate

Darcy's law

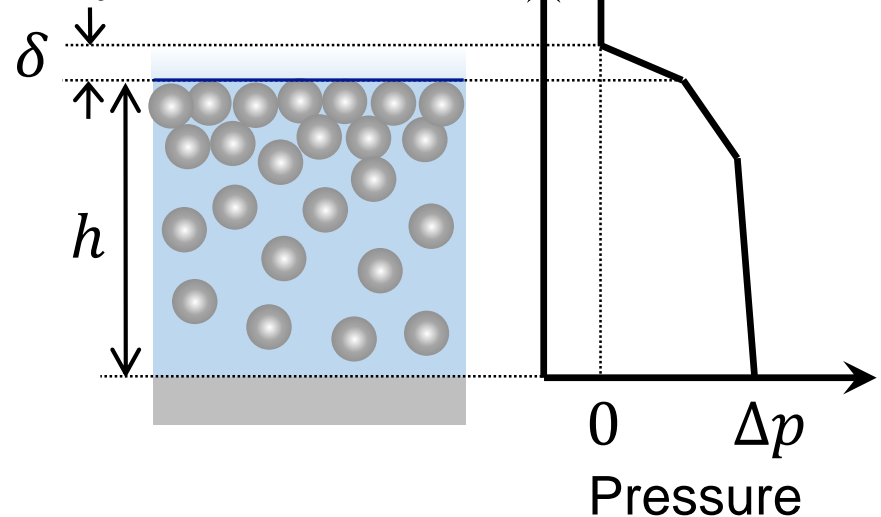
$$\text{Drying rate: } u = \frac{\Delta p}{\eta(R_0 + R_p)}$$

Resistance of evaporation: R_0

Resistance of suspensions: R_p

Viscosity of liquid: η

Boundary film



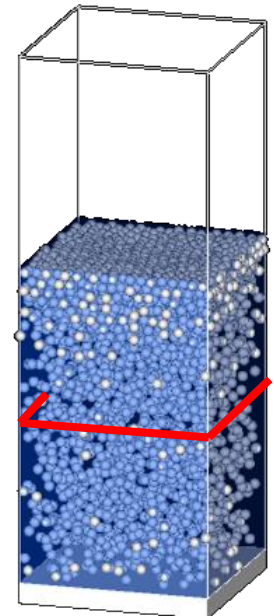
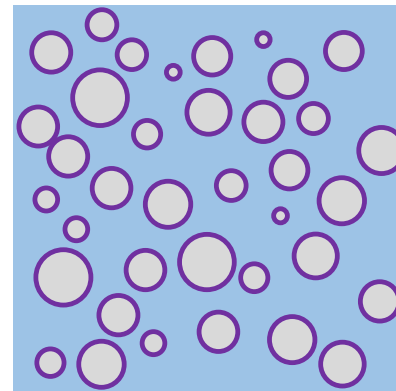
Resistance of suspensions

$$R_p = \int_0^h r(z) dz \quad r(z) = \frac{80}{[D_H(z)]^2} \frac{S_{\text{tot}}}{S_f(z)}$$

Hydraulic diameter: $D_H = \frac{4S_f}{L_f}$

Cross-sectional area of the flow: S_f

Wetted perimeter: L_f



Simulation Conditions

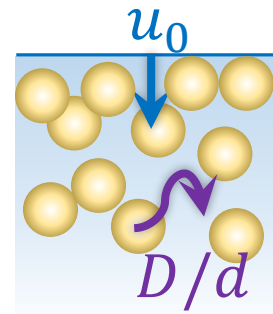
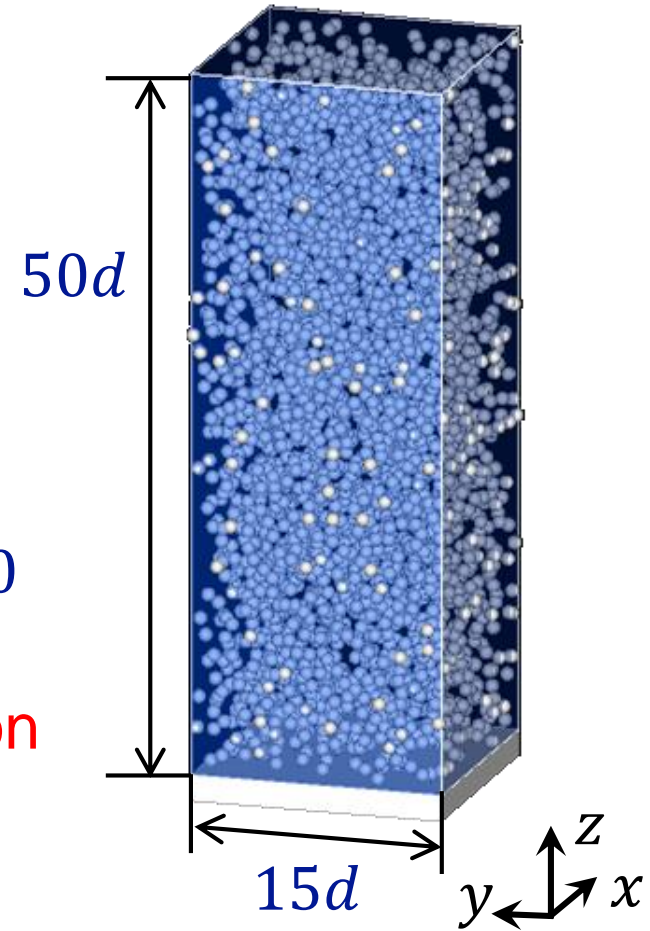
- Particle diameter d
- Initial volume particle fraction 0.1
- Resistance of evaporation $R_0 d = 200$
- Initial particle drying Péclet number

$$Pe_0 = \frac{\text{(Drying rate)}}{\text{(Diffusion rate)}} = \frac{u_0}{D/d} = \frac{u_0 d}{D} = 100$$

- Interparticle force: Dispersion/Aggregation

Corresponding system

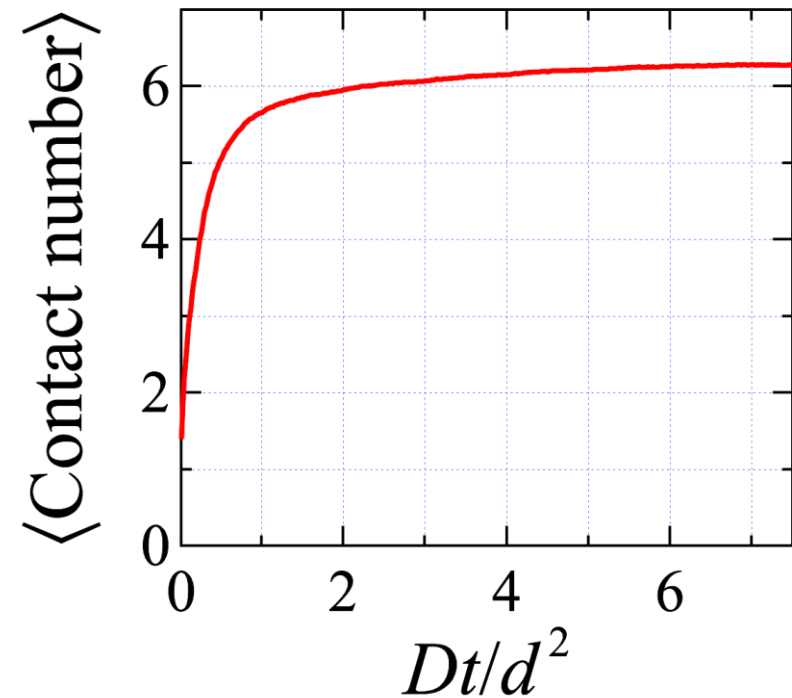
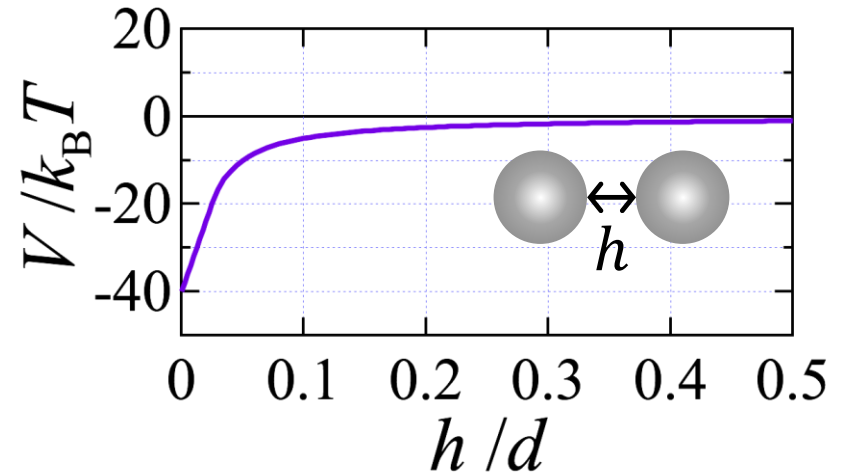
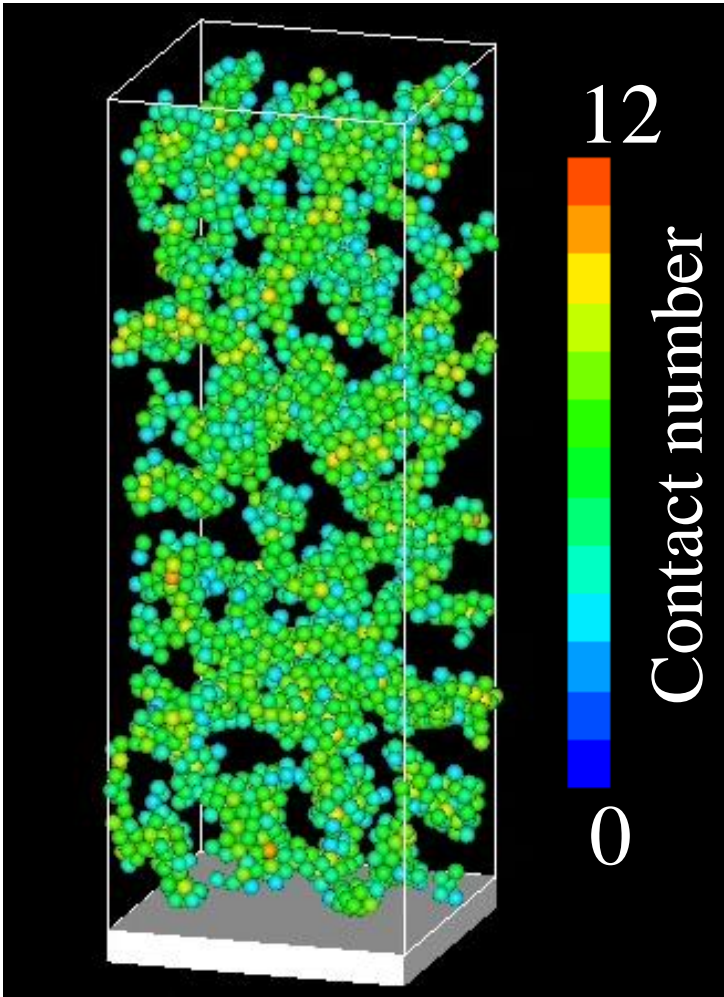
- Particles: $d = 100$ nm
- Medium: Water
- Condition: $T \approx 330$ K,
 $u_0 \approx 5 \times 10^{-3}$ m/s



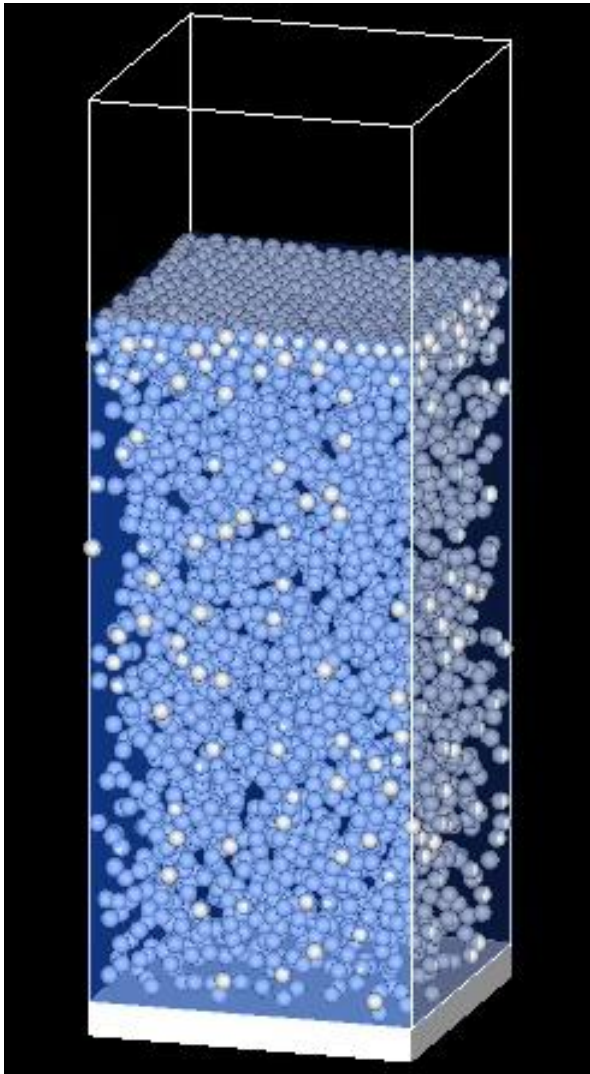
Periodic boundaries: x, y

Aggregation

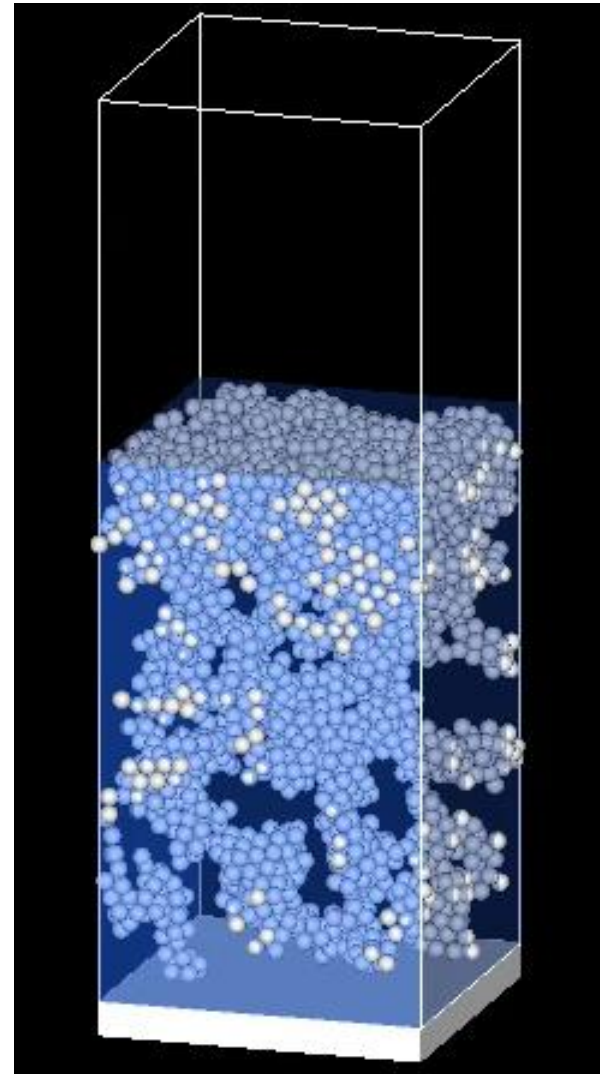
Van der Waals potential
between particles



Particle Distribution

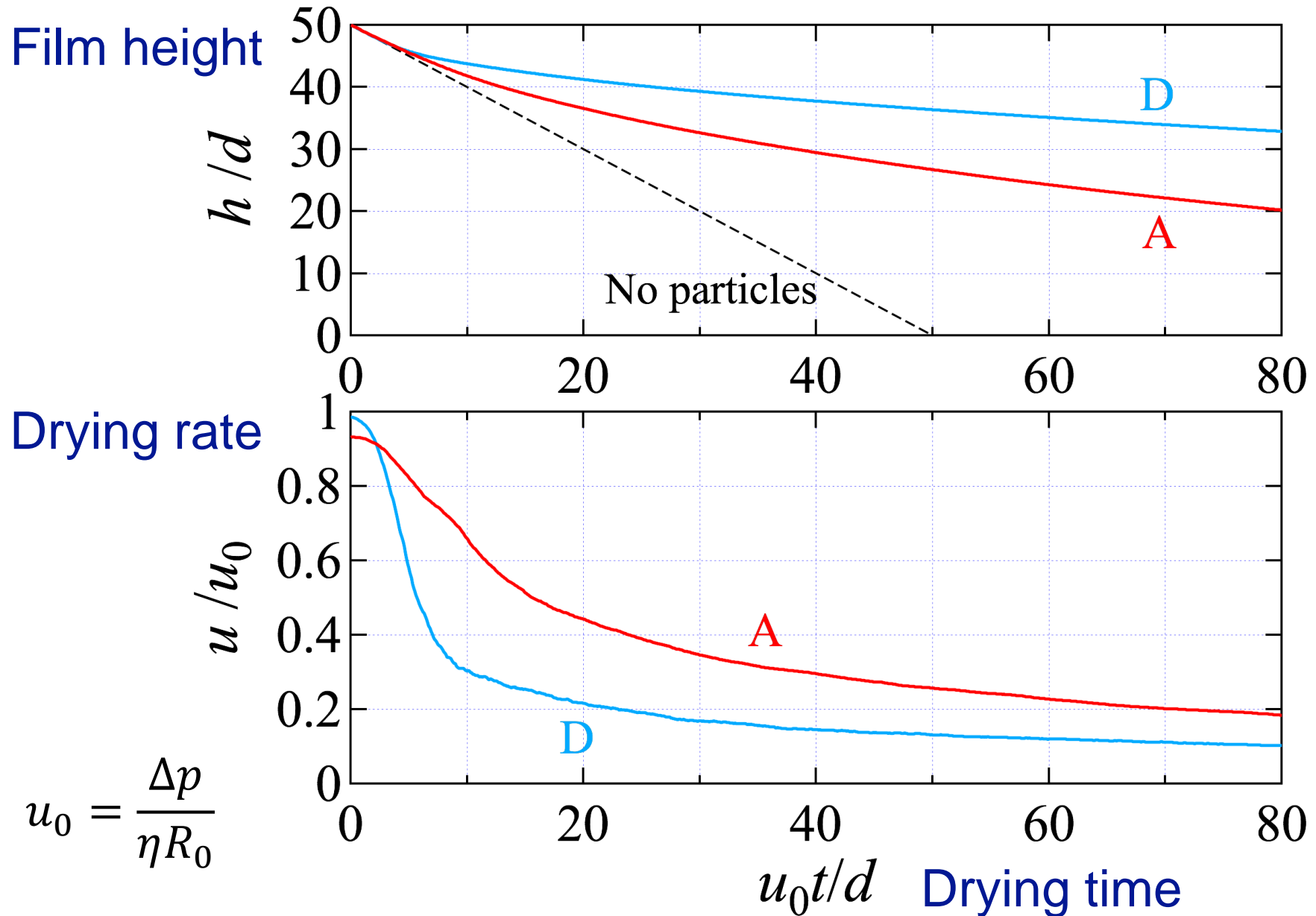


Dispersion

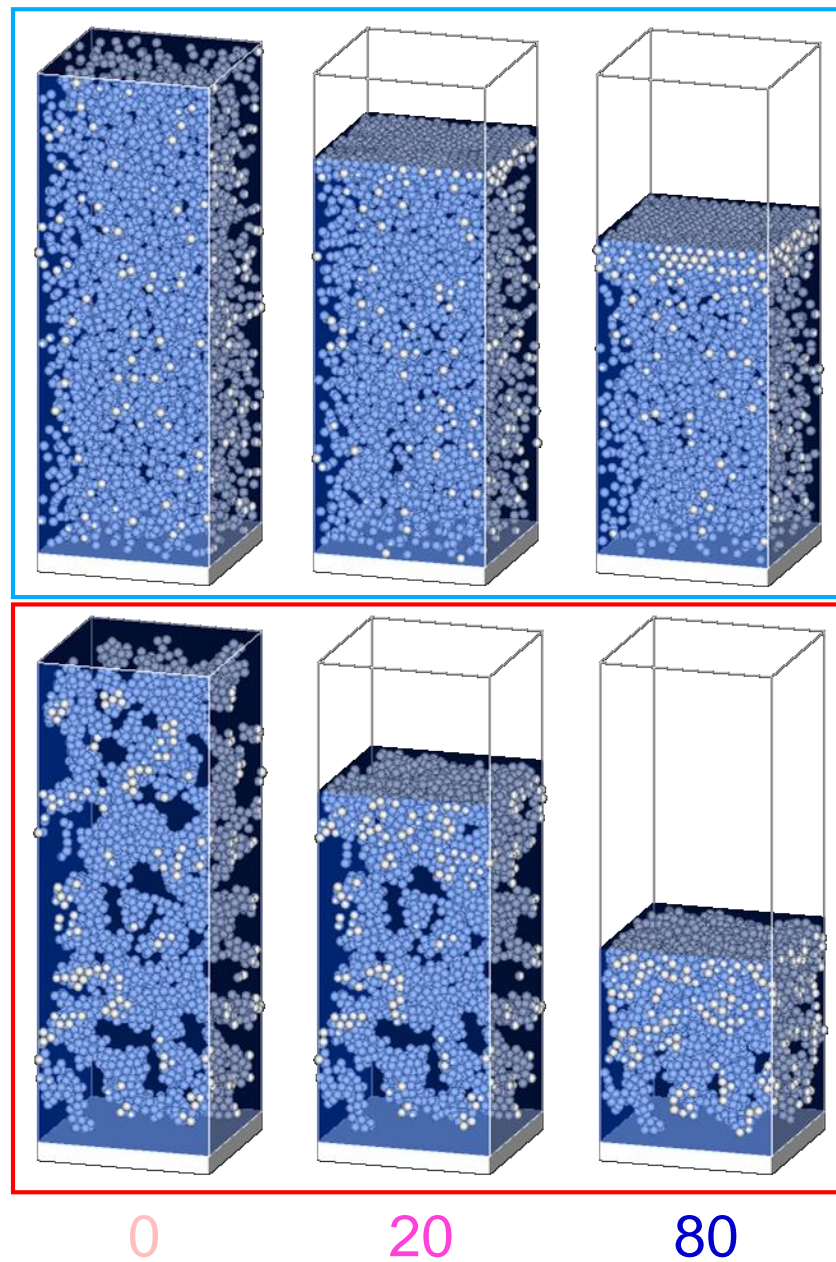
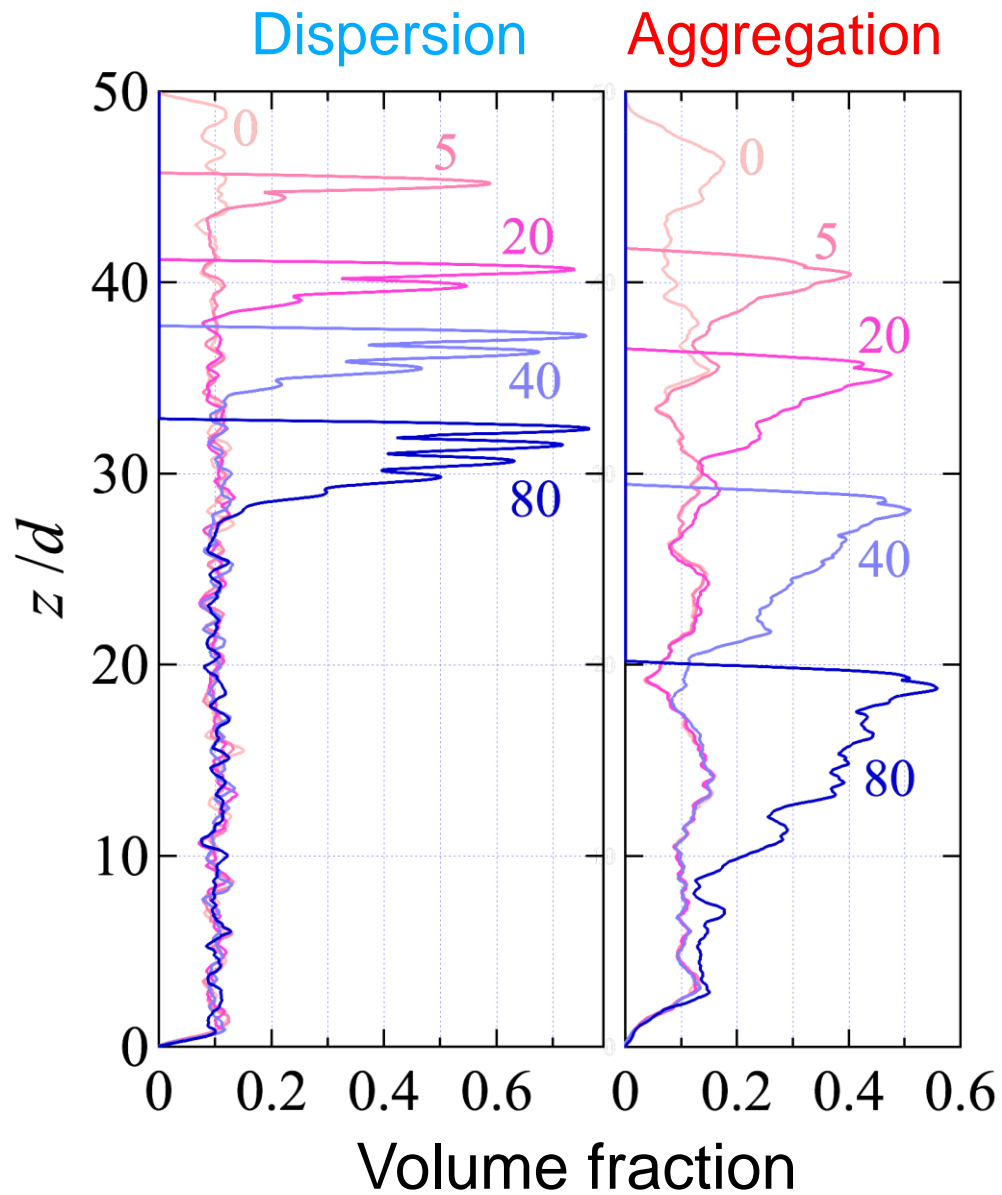


Aggregation

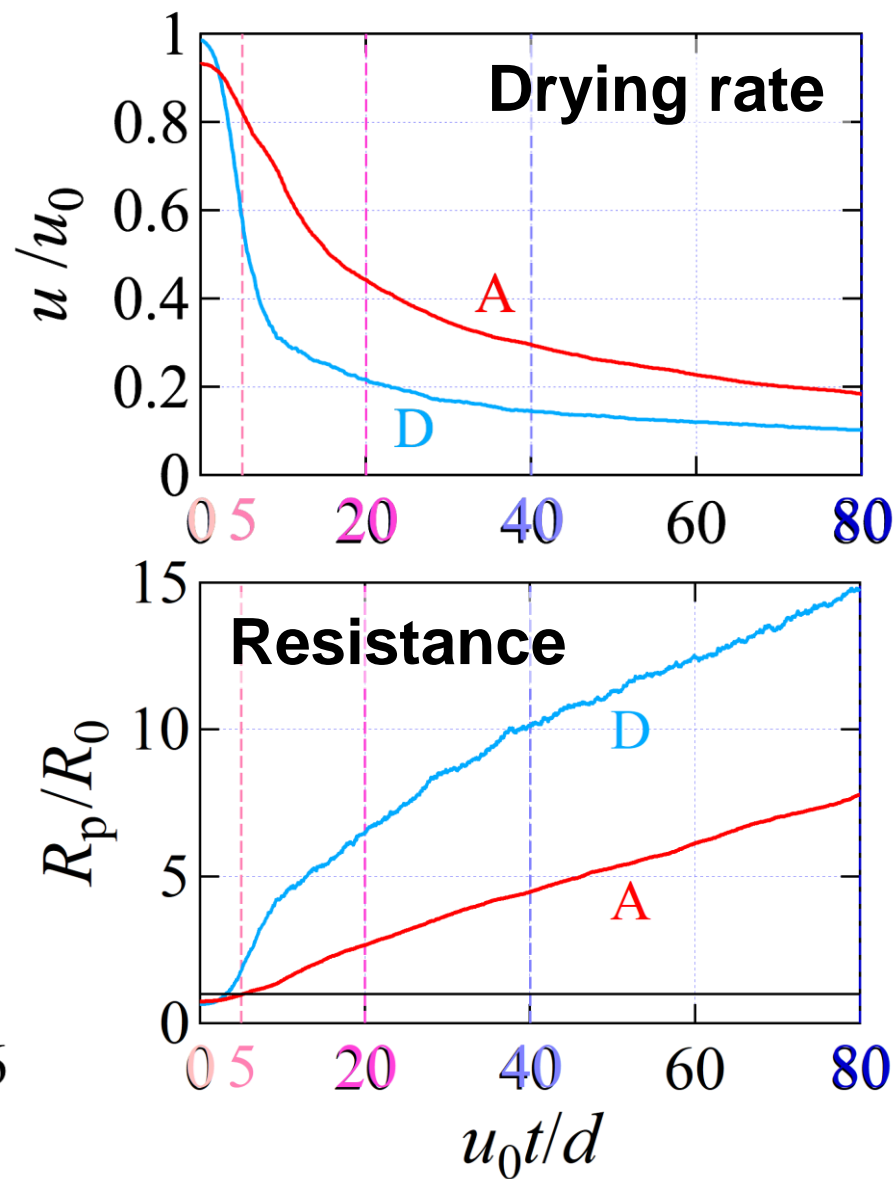
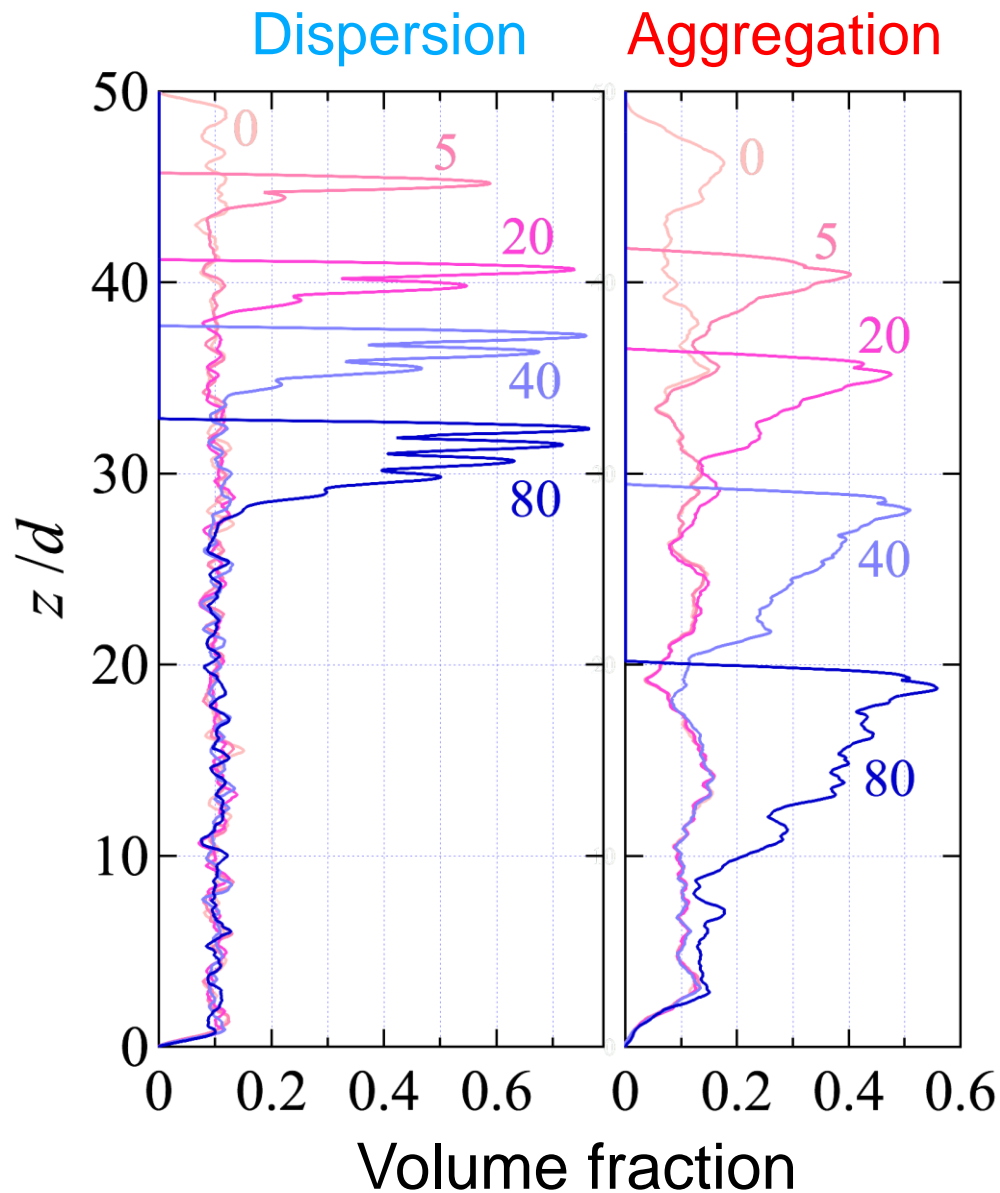
Drying Characteristics



Particle Distribution



Particle Distribution



Summary

- ◆ Model to estimate the drying characteristics:

$$u = \frac{\Delta p}{\eta(R_0 + R_p)}$$

- ◆ Effects of particle dispersion/aggregation on the drying characteristics
 - Aggregation: higher porosity → higher drying rate
 - Dispersion/aggregation control to reduce drying time